

AD A119959

DTIC FILE COPY

②

NRL Report 8627

## Computing the Grazing Angle of Specular Reflection

A. MILLER

*Software Systems and Support Branch  
Research Computation Division*

E. VEGH

*Identification Systems Branch  
Radar Division*

September 21, 1982



DTIC  
OCT 5 1982  
A

NAVAL RESEARCH LABORATORY  
Washington, D.C.

Approved for public release; distribution unlimited.

82 10 05 097

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NRL Report 8627	2. GOVT ACCESSION NO. AD-A119939	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) COMPUTING THE GRAZING ANGLE OF SPECULAR REFLECTION	5. TYPE OF REPORT & PERIOD COVERED Final report	
7. AUTHOR(s) A. Miller and E. Vegh	6. PERFORMING ORG. REPORT NUMBER	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Research Laboratory Washington, DC 20375	8. CONTRACT OR GRANT NUMBER(s)	
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Air Systems Command Washington, DC 20361	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS PE 62712N, WF1214000 53-0660-02	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)	12. REPORT DATE September 21, 1982	
	13. NUMBER OF PAGES 10	
	15. SECURITY CLASS. (of this report) UNCLASSIFIED	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Grazing angle Specular reflection Iterative procedures Contraction mapping Spherical earth FORTRAN		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Three methods for computing the grazing angle of specular reflection are given. A FORTRAN program that employs one of the methods and computes the grazing angle to an arbitrary degree of accuracy is also provided.		

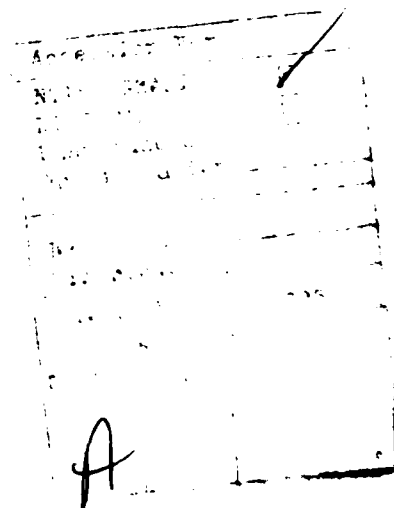
DD FORM 1473  
1 JAN 73

EDITION OF 1 NOV 65 IS OBSOLETE  
S/N 0102-014-6601

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

## CONTENTS

INTRODUCTION .....	1
GENERAL REMARKS .....	1
METHOD ONE .....	2
METHOD TWO .....	2
METHOD THREE .....	3
CONCLUSION .....	3
REFERENCES .....	3
APPENDIX A — Proof of Convergence to the Grazing Angle .....	5
APPENDIX B — A FORTRAN Program of Method Two .....	7
APPENDIX C — Derivation of the Quartic .....	8



# COMPUTING THE GRAZING ANGLE OF SPECULAR REFLECTION

## INTRODUCTION

In this report we give three methods for computing the grazing angle of specular reflection. The first was developed by Fishback [1,2] in 1943 and refined somewhat by Blake [3] in 1980, and it gives an approximation to the grazing angle. The second is an iterative method, whose derivation is easy and provides for the computation of the grazing angle to any degree of accuracy specified. The third method shows that there is a closed form explicit expression for the grazing angle. This in turn also allows for a computation to an arbitrary degree of accuracy. A FORTRAN program of the second method is included in Appendix B.

## GENERAL REMARKS

The geometry of the spherical-earth problem and definitions of various angles and distances are given in Fig. 1.

The problem of computing the grazing angle of specular reflection is that of computing  $\psi$  in Fig. 1, i.e., finding  $\psi$  an angle between the tangent line,  $l$ , to the circle and  $\overline{AR}$  where  $\psi$  is also the angle between  $l$  and  $\overline{TR}$ .

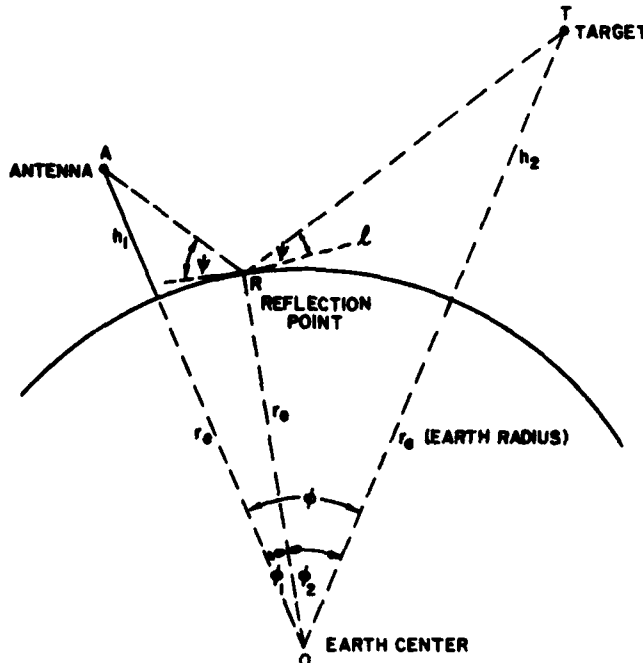


Fig. 1 — Geometry of spherical-earth specular reflection

We assume that  $\phi = (\phi_1 + \phi_2)$ ;  $h_1$ ,  $h_2$ , and  $r_e$  are given. Define  $k_i = \frac{r_e}{r_e + h_i}$ ,  $i = 1, 2$ .

### METHOD ONE

In method one, let

$$s = r_e \phi, \quad (1)$$

$$p^2 = \frac{4}{3} \left[ r_e (h_1 + h_2) + \frac{1}{4} s^2 \right], \quad (2)$$

and

$$q = \sin^{-1} \left[ 2p^{-3} r_e s (h_2 - h_1) \right]. \quad (3)$$

Then when  $h_1$  and  $h_2$  are very much less than  $r_e$ , Fishback approximates  $\phi_1$  by

$$\phi_1 \doteq \frac{1}{2} \phi - \frac{p}{r_e} \sin \left[ \frac{q}{3} \right]. \quad (4)$$

Finally, the grazing angle  $\psi$  is given by

$$\psi = \tan^{-1} (\cot \phi_1 - k_1 \csc \phi_1). \quad (5)$$

The error in the approximation for  $\phi_1$  (and consequently for  $\psi$ ) is not generally known. However, if  $h_1 = h_2$ , then  $\phi_1 = 1/2\phi$  and Eq. (5) provides the exact result for the grazing angle.

### METHOD TWO

Method two uses an iterative procedure for computing the grazing angle to any degree of accuracy.

First, applying the law of sines to triangles OAR and ORT, we obtain

$$\phi_1 + \psi = \cos^{-1} (k_1 \cos \psi) \quad (6)$$

and

$$\phi_2 + \psi = \cos^{-1} (k_2 \cos \psi). \quad (7)$$

Adding the equations (and recalling that  $\phi = \phi_1 + \phi_2$ ) we have,

$$\psi = g(\psi) \quad (8)$$

where,

$$g(\psi) = \frac{1}{2} \left[ \cos^{-1} (k_1 \cos \psi) + \cos^{-1} (k_2 \cos \psi) - \phi \right]. \quad (9)$$

If we choose  $\psi_0$  arbitrarily and define

$$\psi_{i+1} = g(\psi_i), \quad i = 0, 1, 2, \dots \quad (10)$$

then by the results of Appendix A,

$$\lim_{i \rightarrow \infty} \psi_i \quad (11)$$

exists and is the unique solution of Eq. (8), i.e., (11) is the grazing angle.

Approximations to the grazing angle are given by the terms of the sequence  $\psi_0, \psi_1, \dots$ , with successive terms providing more accurate approximations. In practice, when the relative difference of successive terms of this sequence differ in absolute value by no more than a predetermined constant, we obtain the grazing angle to our required degree of accuracy. A FORTRAN program implementing method two is given in Appendix B.

To obtain a rapid convergence for method two, we might use method one to obtain the initial value,  $\psi_0$ . In addition, method two may be useful in real-time computation of the grazing angle, since an angle once computed may be used as the initial value for an update computation.

### METHOD THREE

The third method produces, in principle, an explicit expression for the grazing angle.

Let  $U = \exp(i\phi)$  and  $Z = \exp(2i\psi)$ .

Then replacing  $U$  and  $Z$  in Eq. (8), we obtain the following quartic (see Appendix C for derivation):

$$\alpha Z^4 + \beta Z^3 + CZ^2 + \bar{\beta}Z + \bar{\alpha} = 0, \quad (12)$$

where,

$$A = U - k_1 k_2,$$

$$\alpha = UA,$$

$$\beta = k_1^2 + k_2^2 - 2k_1 k_2 U,$$

and

$$C = 2\text{Re}[\beta - U\bar{A}].$$

Since Eq. (12) is a quartic, the roots can be exhibited explicitly using the classical method of Ferrari and Cardan [4]. At least one of these roots lies on the unit circle. Let  $Z_0$  designate any of those roots on the unit circle. Then

$$\psi_0 \equiv \frac{1}{2} \cos^{-1} \{\text{Re}(Z_0)\}, \quad (13)$$

and that unique value of  $\psi_0$  that satisfies Eq. (8) is the grazing angle.

Rather than use the method of Ferrari and Cardan to find the four roots of Eq. (12), it is easier and more efficient to solve the quartic numerically on a computer using a polynomial root finder routine.

### CONCLUSION

Three methods for computing the grazing angle of specular reflection are given. The first provides an approximation where the error is not known. Methods two and three will provide computations good to any degree of accuracy. Method two, an iterative procedure, may be especially useful in real time computation.

### REFERENCES

1. W.T. Fishback, "Simplified Methods of Field Intensity Calculations in the Interface Region," Report 461, Radiation Laboratory, M.I.T., December 1943.

MILLER AND VEGH

2. D.E. Kerr, *Propagation of Short Radio Waves*, McGraw-Hill Book Co., N.Y., 1951.
3. L.V. Blake, *Radar Range-Performance Analyses*, Lexington Books, Lexington, Mass., 1980.
4. G.A. Korn and T.M. Korn, *Mathematical Handbook for Scientists and Engineers*, McGraw-Hill Book Co., 1968.

## Appendix A

### PROOF OF CONVERGENCE TO THE GRAZING ANGLE

Let  $X$  be an arbitrary set,  $d$  a metric on  $X$ , and  $f$  a contraction mapping of  $X$  to itself. ( $f$  is called a contraction mapping if there is a positive constant  $k < 1$  such that

$$d(f(x), f(y)) \leq k d(x, y) \text{ for all } x, y \text{ in } X).$$

The following result may be found in [A1].

**THEOREM:** Every contraction mapping,  $f$ , on a complete metric space has a unique fixed point, i.e., there is a unique  $x$  in  $X$  such that  $f(x) = x$ . Furthermore, for an arbitrary  $x_0$  in  $X$ , the sequence given by  $x_{n+1} = f(x_n)$ ,  $n = 0, 1, 2, \dots$  converges to  $x$ .

As a special case, let  $X$  be the reals and for  $x, y$  in  $X$  let  $d(x, y) = |x - y|$ . Then  $(X, d)$  is a complete metric space.

Now let  $f$  be a differentiable function defined on  $X$  and suppose furthermore that there is a constant  $k$ ,  $0 < k < 1$  such that  $|f'(x)| \leq k$  for all  $x$  in  $X$ . Then  $f$  is a contraction mapping. This may be seen as follows. Let  $x$  and  $y$  be real numbers,  $x < y$ . By the mean value theorem there is a number  $\xi$ ,  $x \leq \xi < y$  such that

$$f(x) - f(y) = (x - y)f'(\xi).$$

Hence,

$$|f(x) - f(y)| = |x - y||f'(\xi)| \leq k |x - y|.$$

These results may be summarized in the following.

**COROLLARY:** Let  $R$  be the reals,  $k$  a constant  $0 < k < 1$ , and  $f$  a differentiable function on  $R$  such that  $|f'(x)| \leq k$  for all  $x$  in  $R$ . Then there is a unique real number  $a$  such that

$$a = f(a).$$

Moreover, if  $x_0$  is an arbitrary real number and  $x_{n+1} = f(x_n)$ ,  $n = 0, 1, 2, \dots$ , then

$$\lim_{n \rightarrow \infty} x_n = a.$$

With respect to Method 2, we have given the differentiable function

$$g(x) = \frac{1}{2} [\cos^{-1}(k_1 \cos x) + \cos^{-1}(k_2 \cos x) - \phi].$$

Differentiating, we have

$$\begin{aligned} 2g'(x) &= \frac{k_1 \sin x}{\sqrt{1 - k_1^2 \cos^2 x}} + \frac{k_2 \sin x}{\sqrt{1 - k_2^2 \cos^2 x}}, \\ &= \pm k_1 \sqrt{\frac{1 - \cos^2 x}{1 - k_1^2 \cos^2 x}} \pm k_2 \sqrt{\frac{1 - \cos^2 x}{1 - k_2^2 \cos^2 x}}. \end{aligned}$$



Recalling that

$$k_i = \frac{r_e}{r_e + h_i} < 1, \quad i = 1, 2$$

we have

$$|2g'(x)| \leq k_1 \sqrt{\frac{1 - \cos^2 x}{1 - k_1^2 \cos^2 x}} + k_2 \sqrt{\frac{1 - \cos^2 x}{1 - k_2^2 \cos^2 x}}$$

$$\leq k_1 + k_2 < 2,$$

or

$$|g'(x)| \leq \frac{k_1 + k_2}{2} < 1.$$

Hence, by the Corollary, there is a unique number  $a$  such that

$$a = g(a).$$

Moreover, if  $x_0$  is arbitrary and  $x_{n+1} = g(x_n)$ ,  $n = 0, 1, 2, \dots$ , then

$$\lim_{n \rightarrow \infty} x_n = a.$$

#### REFERENCE

- A1. G. Bachman and L. Narici, *Functional Analysis*, Academic Press, N.Y., 1966.

Appendix B  
A FORTRAN PROGRAM OF METHOD TWO

SOURCE LISTING                      ASC FAST FORTRAN COMPILER                      RELEASE FTFX0529.P294/RC  
STATEMENT                              CP OPTIONS = (M,X)                      DATE = 05/06/82(R2.126)

```

SUBROUTINE GRAZE(H1,H2,THETA,RE,PHI)
C
C   THIS ROUTINE COMPUTES THE GRAZING ANGLE PHI FOR SPHERICAL
C   EARTH SPECULAR REFLECTION.
C
C   H1= ANTENNA HEIGHT.
C   H2= TARGET HEIGHT.
C   RE= EARTH EFFECTIVE RADIUS OR EARTH RADIUS.
C   THETA IS CENTRAL ANGLE IN RADIAN.
C
C   PHI MUST BE INITIALIZED IN CALLING ROUTINE: PHI .NE. 0.
C   PHIT= GRAZING ANGLE OUTPUT IN RADIAN.
C   RELATIVE ERROR IN PHI IS 10**-8, BUT CAN BE DECREASED BY CHANGING
C   VALUE OF TOL IN DATA STATEMENT.
C
C   INPUTS AND OUTPUTS ARE IN REAL*8: REAL*4 CAN BE USED BY REMOVING
C   IMPLICIT STATEMENT AND ADJUSTING TOL.
C
C   H1, H2, RE, THETA ARE INPUTS. UNITS FOR H1, H2, RE MUST BE
C   CONSISTENT.
C
C   IMPLICIT REAL*8(A-H,I-Z)
C
C   DATA TOL/1.0D-8/
C
C   RK1=RE/(H1+RE)
C   RK2=RE/(H2+RE)
C
C   A=0ARCOS(RK1)+0ARCOS(RK2)-THETA
C   IF( A .GE. 0.0D0 .AND. A .LE. 1.0D-15 ) GOTO 11
20  G=0.500*(0ARCOS(RK1+DCOS(PHI)) + 0ARCOS(RK2+DCOS(PHI)) - THETA)
C
C   RTST=(G-PHI)/PHI
C   RTST=0ABS(RTST)
C
C   IF(RTST.LE. TOL ) GOTO 10
C
C   PHIT=G
C
C   GOTO 20
C
10  PHIT=G
C
C   RETURN
C
11  PHIT=0.0D0
C   RETURN
C   END

```

### Appendix C

#### DERIVATION OF THE QUARTIC

Beginning with Eq. (8), we have

$$\cos(2\psi + \phi) = k_1 k_2 \cos^2 \psi - \sqrt{1 - k_1^2} \cos^2 \psi \sqrt{1 - k_2^2} \cos^2 \psi.$$

Squaring, we obtain

$$(1 - k_1^2 \cos^2 \psi)(1 - k_2^2 \cos^2 \psi) = [k_1 k_2 \cos^2 \psi - \cos(2\psi + \phi)]^2,$$

or

$$1 - (k_1^2 + k_2^2) \cos^2 \psi = \cos^2(2\psi + \phi) - 2k_1 k_2 \cos^2 \psi \cos(2\psi + \phi). \quad (C1)$$

Let  $U = \exp(i\phi)$  and  $Z = \exp(i2\psi)$ ,

so that

$$\cos^2 \psi = \frac{1}{4}(Z + \bar{Z} + 2),$$

and

$$\cos(2\psi + \phi) = \frac{1}{2}[UZ + \bar{U}\bar{Z}]. \quad (C3)$$

Multiplying both sides of Eq. (C1) by  $4U^2 Z^2$  and substituting Eq. (C2) and Eq. (C3) into Eq. (C1) we have

$$\begin{aligned} 4U^2 Z^2 - U^2(k_1^2 + k_2^2)(Z^3 + 2Z^2 + Z) \\ = (U^4 Z^4 + 2U^2 Z^2 + 1) - Uk_1 k_2 (Z^2 + 2Z + 1)(U^2 Z^2 + 1). \end{aligned}$$

Then grouping the terms in powers of  $Z$  gives

$$U^3 A Z^4 + U^2 \beta Z^3 + U^2 (2\operatorname{Re}(\beta - U\bar{A})) Z^2 + U^2 \bar{\beta} Z + U\bar{A} = 0.$$

Now dividing by  $U^2$  gives Eq. (12).